

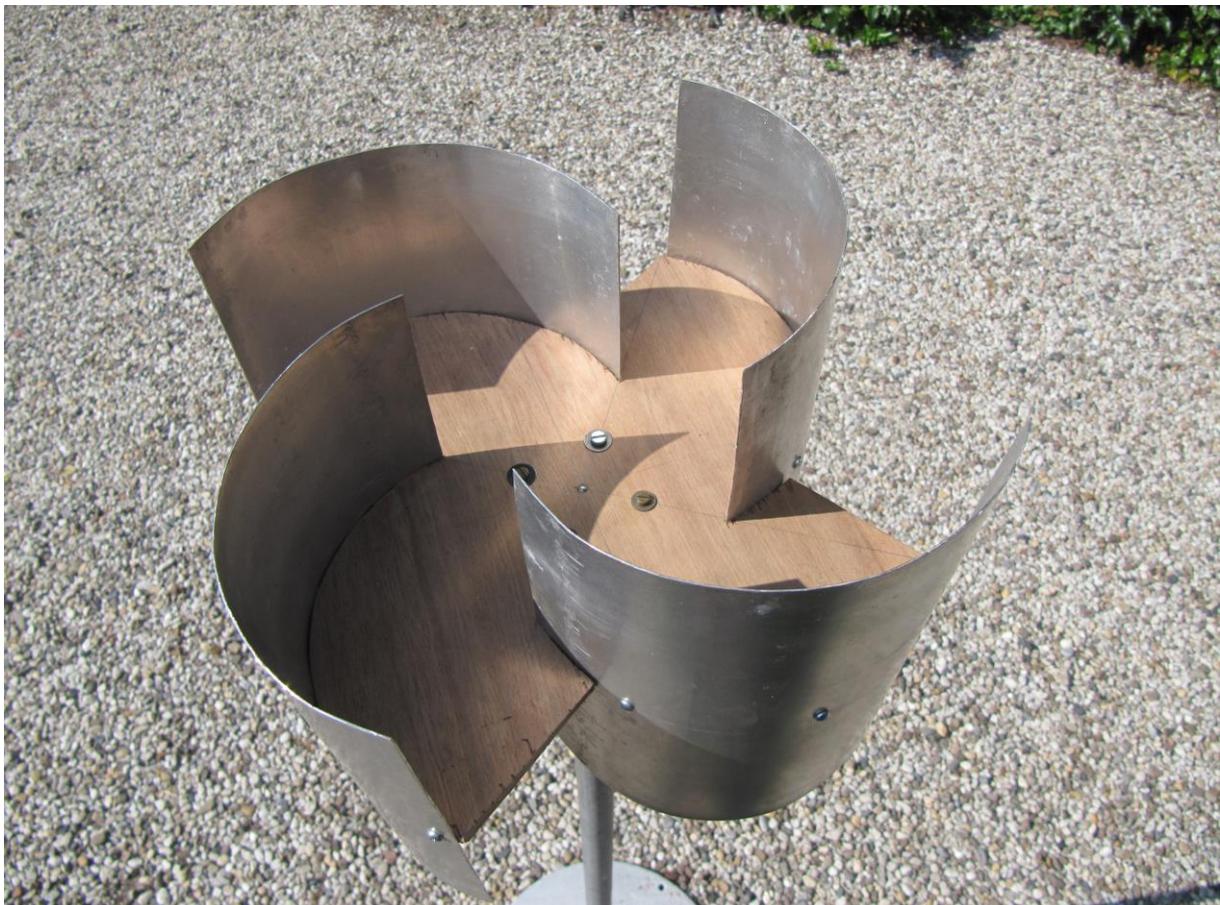
**Ideas about a 4-buckets Savonius rotor called the VIRYA-1.45  
for driving a positive displacement pump**

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The idea of this rotor can be used by anyone but the VIRYA-1.45 rotor or a proper scale model of it has not yet been built and tested. Especially because the windmill has no safety system, no responsibility is accepted by Kragten Design by use of this rotor.



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## 1 Introduction

A normal Savonius rotor is a vertical axis wind turbine (VAWT) with two buckets made out of a half cylinder. The cylinders have a certain overlap and this overlap allows an internal flow through the rotor. Because of this internal flow, a Savonius rotor is not a pure drag machine but during a part of a revolution it also works as a lift machine. Therefore it has a higher maximum  $C_p$  than a pure drag machine. Information about pure drag machines is given in my public report KD 416 (ref. 1). Information about measurements on Savonius rotors available on the Internet is given in my public report KD 599 (ref. 2).

The starting torque of a normal Savonius rotor depends very much on the position of the buckets with respect to the wind direction. The starting torque is maximal if the buckets are perpendicular to the wind and almost zero if the buckets are in line with the wind direction. Several methods are used to solve this problem. The most common method is to use two Savonius rotors on top of each other which are  $90^\circ$  rotated with respect to each other. Such a Savonius rotor is also called a 2-phase Savonius rotor. Another option is to give the blades a  $90^\circ$  twist but manufacture of such blades is rather difficult. One has also tried to make Savonius rotors with three buckets but those rotors have a very low maximum  $C_p$  because there is almost no flow through the rotor. There is certainly no flow at all if the three buckets touch each other at the centre of the rotor.

Some time ago the idea came up to design a Savonius rotor with four buckets and to do it such that there is enough space in the centre of the rotor for an internal flow. The starting torque will fluctuate only a little if four buckets are used. The rotor will therefore have a high starting torque coefficient and will therefore be able to drive a positive displacement pump. As the rotor has a vertical axis, the pump can be coupled directly to the rotor axis if the correct pump type and pump geometry is chosen. Selection of the correct pump is out of the scope of this report. For generation of electricity, I will always advice to use a horizontal axis wind turbine (HAWT) as such a wind turbine uses much less material for a certain power.

## 2 Description of the rotor of the 4-buckets Savonius rotor

An important point for the rotor geometry is optimal use of materials. It was chosen to use stainless steel or galvanised steel with dimensions  $1000 * 1000 * 1$  mm for one bucket. So two sheets of  $1 * 2$  m are needed for four buckets. A sheet is cambered such that it covers an angle of  $135^\circ$  (the bucket of a normal Savonius rotor covers an angle of  $180^\circ$ ). Because of the  $135^\circ$  angle, there is a square area in the heart of the rotor where there are no buckets. The camber radius  $r$  for a sheet length  $l$  can be calculated by the formula:

$$r = l * 360 / (2\pi * 135) \quad (\text{mm}) \quad (1)$$

Substitution  $l = 1000$  mm in formula 1 gives that  $r = 424.4$  mm. The square area in the centre of the rotor has sides with a width of 424.4 mm. These sides make an angle of  $45^\circ$  with the lines through the tips of the buckets. The distance  $a$  in between the corner of the square area and the heart of the rotor is therefore  $424 / \sqrt{2} = 300.1$  mm. For the rotor radius  $R$  we therefore find that  $R = r + a = 424.4 + 300.1 = 724.5$  mm. The rotor diameter  $D$  is two times  $R$  and so  $D = 2 * 724.5 = 1449$  mm. This is at the heart of the 1 mm thick sheet. So at the outside of the sheet, the diameter  $D$  is  $1450$  mm =  $1.45$  m and the rotor is therefore called the VIRYA-1.45. The rotor has a height  $H$  of  $1000$  mm =  $1$  m and the swept rotor area  $A$  is therefore  $1 * 1.45 = 1.45$  m<sup>2</sup>. The total blade area is  $4$  m<sup>2</sup> so the solidity is  $4 / 1.45 = 2.759$ .

The four buckets are connected to each other by one 18 mm thick water proof plywood sheet which is mounted just half way the height of the rotor. Two sheets can be made out of a standard sheet size  $1.22 * 2.44$  m. Each blade is connected to the sheet by a large number of stainless steel screws. A top and a side view of the rotor are given in figure 1.

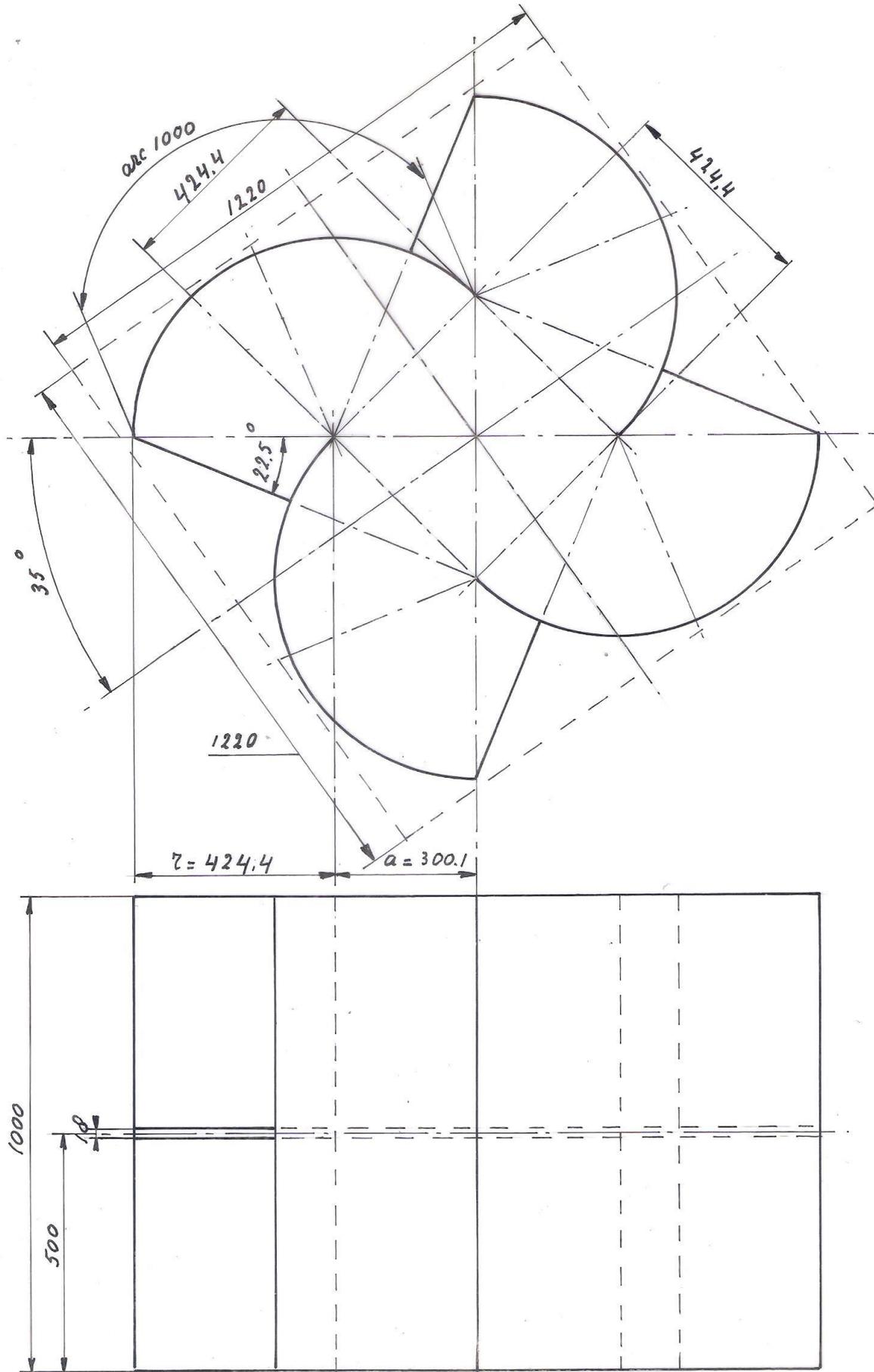


Figure 1 Sketch of the VIRYA-1.45, 4-buckets Savonius rotor

In stead of a plywood sheet one can also make a construction of bended and welded strips. Another option is to use a plywood sheet at the top and at the bottom of the rotor. This will result in a higher maximum  $C_p$  because the tip losses will be less. However, now the tower pipe will end at the bottom sheet of the rotor and the bending moment in the rotor shaft will be much larger than for a tower pipe which ends half way the rotor height.

This windmill has no safety system which limits the rotational speed and the rotor thrust at high wind speeds. So this windmill can only be used at sites where very high wind speeds simply don't occur or if the whole windmill is laid down in case of a heavy storm warning!

### 3 Determination of the rotor characteristics

The aerodynamic theory which is given in my public report KD 35 (ref. 3) for HAWT's can't be used to predict the characteristics of this 4-bucket Savonious rotor. The best way is to make a scale model and test it on front of the open wind tunnel like the one of the University of Delft. However, these tests will be rather expensive if the wind tunnel has to be hired. Another way is to test a scale model in the open air.

Assume the original rotor is scaled down with a factor 2. This means that now the buckets are made of sheet size 500 \* 500 \* 0.5 mm and that the plywood sheet is made from a sheet size 610 \* 610 \* 9 mm. So now the rotor diameter  $D$  is 0.725 m and the rotor height  $H = 0.5$  m. The swept rotor area  $A$  is now 0.3625 m<sup>2</sup>.

I have measured a Chinese axial flux PM-generator for which the characteristics for 12 V battery charging are given in public report KD 595 (ref. 4). Assume that this generator is used to test a scale model of the VIRYA-1.45 rotor. The plywood sheet is connected to the generator housing by six bolts M8 at a pitch circle of 65 mm. It isn't sure if the maximum torque level of this generator is high enough to load the rotor strong enough but at least some information about the behaviour can be gained. If the generator appears to be not strong enough, one has to take a bigger one. Kragten Design will perform no tests for this windmill.

The photo on the front page is from a very simple scale model scale 1 : 5 using 0.8 mm thick aluminium blades. I have tested this rotor on a bicycle. The rotor runs nicely unloaded but this says nothing about its characteristics.

### 4 References

- 1 Kragten A. Windmills using aerodynamic drag as propelling force; a hopeless concept, April 2009, reviewed September 2019, free public report KD 416, engineering office Kragten Design, Populierenlaan 51, 5492 SG Sint-Oedenrode, The Netherlands.
- 2 Kragten A. Measurements of Savonious rotors available on the Internet, December 2009, reviewed Augustus 2019, free public report KD 599, engineering office Kragten Design, Populierenlaan 51, 5492 SG Sint-Oedenrode, The Netherlands.
- 3 Kragten A. Rotor design and matching for horizontal axis wind turbines, January 1999, reviewed February 2017, free public rapport KD 35, engineering office Kragten Design, Populierenlaan 51, 5492 SG Sint-Oedenrode, The Netherlands.
- 4 Kragten A. Measurements performed on a Chinese axial flux generator of Hefei Top Grand model TGET165-0.15kW-500R for a 12 V battery load, September 2015, free public report KD 595, engineering office Kragten Design, Populierenlaan 51, 5492 SG Sint-Oedenrode, The Netherlands.